Hydraulic jump Harald Hanche-Olsen hanche@math.ntnu.no

This little note is a supplement to the next-to-last part of the course notes, pp. 43–48. I am not going to rederive the equations here. (But I will remark that life becomes a little bit simpler if you chose $\theta_0 = \pi/2$ in the control volume for the impulse balance.

The mass balance and impulse balance become equations (190) and (196) in the compendium (in compact but hopefully unambiguous notation):

$$\frac{\mathrm{d}}{\mathrm{d}t} \int_{r_1}^{r_2} hr \,\mathrm{d}r + \left[rhv\right]_{r_1}^{r_2} = 0,$$
$$\frac{\mathrm{d}}{\mathrm{d}t} \int_{r_1}^{r_2} rhv \,\mathrm{d}r + \left[rhv^2 + \frac{1}{2}grh^2\right]_{r_1}^{r_2} = \int_{r_1}^{r_2} \left(\frac{1}{2}gh^2 - C_fv^2r\right) \mathrm{d}r.$$

Assuming stationary flow, we throw away the first term in each equation (with the time derivative). Further ignoring the friction term (i.e., setting $C_f = 0$) and assuming a smooth solution, we end up with the two equations

$$(rh\nu)' = 0, (1)$$

$$(rhv^2 + \frac{1}{2}grh^2)' = \frac{1}{2}gh^2$$
(2)

where the prime means differentiation with respect to *r*.

With all these assumptions, Bernoulli's law really should be built into these equations. And it is!

First, note that the first term in (2) is $(rhv^2)' = (rhv)'v + rhvv' = rhvv'$ by the product rule and (1).

Second, note that that the second term is $(\frac{1}{2}grh^2)' = \frac{1}{2}gh^2 + grhh'$ which partially cancels the right hand side of (2), and we are left with rhvv' + grhh' = 0. After dividing by rh, we are left with

$$(\frac{1}{2}\nu^2 + gh)' = 0 \tag{3}$$

which really is Bernoulli's law applied to a streamline either following the surface or the bottom of the flow.

The two equations (1) and (3) can be integrated to yield

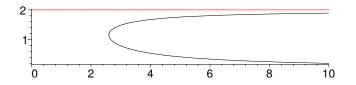
$$rhv = M, \quad v^2 + 2gh = E \tag{4}$$

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for constants *M* (the total volumetric flow, divided by 2π) and *E* (twice the energy per unit mass of the flow). From the first equation we get h = M/(rv) which we substitute into the second, getting $v^2 + 2gM/(rv) = E$. Perhaps more usefully, we write this as

$$\frac{2gM}{r} = (E - v^2)v,\tag{5}$$

and plot the result as follows, with *r* along the horisontal axis and *v* on the vertical axis. (I have arbitrarily plotted the graph with E = 2 and 2gM = 1. Obviously, the general graph is a rescaled version of this one.)



We note that there are two solutions for a given (big enough) *r*: We might call the upper one the *fast* solution and the lower one the *slow* solution. It seems reasonable to expect that fast solution to be appropriate *inside*, and the slow one *outside* the hydraulic jump.

Differentiation the righthand side of (5) wrt v we see that the turning point is at $v = (\frac{1}{3}E)^{1/2}$.

It is useful to express this in terms of the *Froude number*

$$\mathrm{Fr} = \frac{v}{(gh)^{1/2}}.$$

Recall that $(gh)^{1/2}$ is the *wave speed* for shallow water, so that Fr > 1 means the water flow is faster than the wave speed. Using (4) first, and then (5) to eliminate r we get

$$Fr^{2} = \frac{v^{2}}{gh} = \frac{rv^{3}}{gM} = \frac{2v^{3}}{(E-v^{2})v} = \frac{2v^{2}}{E-v^{2}}$$

so that

$$\operatorname{Fr} > 1 \Leftrightarrow 2v^2 > E - v^2 \Leftrightarrow v > (\frac{1}{3}E)^{1/2},$$

which shows that Fr > 1 on the upper branch of the curve and Fr < 1 on the lower branch.

The jump

We return now to the original equations on integral form. Again, looking for a stationary jump at r we drop the time differentiated terms and let $r_1 \rightarrow r$ from below and $r_2 \rightarrow r$ from the right. The integral vansishes in the limit, and we end up with the two jump conditions (after dividing by the common factor r)

$$h_+v_+ = h_-v_-, \quad h_+v_+^2 + \frac{1}{2}gh_+^2 = h_-v_-^2 + \frac{1}{2}gh_-^2$$
 (6)

One way to solve this is the following trick: Note that

$$\frac{hv^2 + \frac{1}{2}gh^2}{(hv)^{4/3}} = \frac{v^{2/3}}{h^{1/3}} + \frac{1}{2}g\frac{h^{2/3}}{v^{4/3}} = g^{1/3}(\mathrm{Fr}^{2/3} + \frac{1}{2}\mathrm{Fr}^{-4/3})$$

(where we used $v^2/h = gFr^2$). So, in the second equation of (6) we divide the two sides by the 4/3rd power of the respective sides of the first equation, which yields

$$\operatorname{Fr}_{+}^{2/3} + \frac{1}{2}\operatorname{Fr}_{+}^{-4/3} = \operatorname{Fr}_{-}^{2/3} + \frac{1}{2}\operatorname{Fr}_{-}^{-4/3}$$

However $Fr^{2/3} + \frac{1}{2}Fr^{-4/3}$ decreases from ∞ to $\frac{3}{2}$ for $Fr \in (0, 1]$, and increases again to ∞ for $Fr \in [1, \infty)$. Thus to each $Fr_{-} \in (1, \infty)$ there corresponds a unique solution $Fr_{+} \in (0, 1)$, In other words, there is a possible jump from a fast flow to a slow one. (The equations also admit a jump from a slow flow to a fast one, but we don't believe in the physical possibility of such a flow.)

Energy loss. The quantity $e = \frac{1}{2}v^2 + gh$ is the total specific energy of a fluid particle, is preserved along a streamline according to Bernoulli's law. However, it will *not* be preserved across the hydraulic jump. The reason is that the region of the jump is a very turbulent region in which liquids with very different speeds collide, so energy is lost there.

To quantify this we use a trick similar to the one above, noting that

$$\frac{\frac{1}{2}v^2 + gh}{(vh)^{2/3}} = g^{2/3}(\frac{1}{2}\mathrm{Fr}^{4/3} + \mathrm{Fr}^{-2/3})$$

The right hand side will change across the jump, and since the denominator on the left hand side does not change, the numerator must.

Experimenting a bit with Maple leads me to believe that

$$(\frac{1}{2}Fr^{4/3} + Fr^{-2/3}) - (Fr^{2/3} + \frac{1}{2}Fr^{-4/3})$$

is a strictly increasing function of Fr. Therefore, since $Fr^{2/3} + \frac{1}{2}Fr^{-4/3}$ is preserved across the jump, the energy will decrease (or increase) across the jump if and only if Fr decreases (or increases).

Indeed, with the shorthand notation $x = Fr^{2/3}$ we get

$$\frac{\mathrm{d}}{\mathrm{d}x} \left(\left(\frac{1}{2}x^2 + x^{-1}\right) - \left(x + \frac{1}{2}x^{-2}\right) \right) = -x + x^{-2} + 1 - x^{-3}$$
$$= x^{-3}(x^4 - x^3 - x + 1) = x^3(x - 1)(x^3 - 1) > 0$$

when x > 0, $x \neq 1$.